

Development of an open-source thermochemical code

Fundamentals and application to shock turbulence interaction problems in the hypersonic regime

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Málaga | December 15, 2021

Huete: Spanish MCINN and BBVA Foundation (Leonardo Grant)



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Part I

Combustion Toolbox: A MATLAB-GUI based open-source tool
for solving gaseous combustion problems

- Thermochemical codes have been a research field since 1960's.
- Applications to many common combustion systems:
 - TP: tail pipe of a car.
 - HP: combustion chamber.
 - SP: expansion through a nozzle.
 - HP and SP: rocket engines.
- Standard thermochemical codes:
 - NASA's CEA (U.S. release only).
 - CANtera (steep learning curve - new users).

Objectives:

- Encapsulate the thermochemical code in a user-friendly GUI.
- Perform shock calculations at high temperatures (ideal plasmas).



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State in which the concentrations of reactants and products do not have a tendency to change with time.

At constant temperature and pressure:

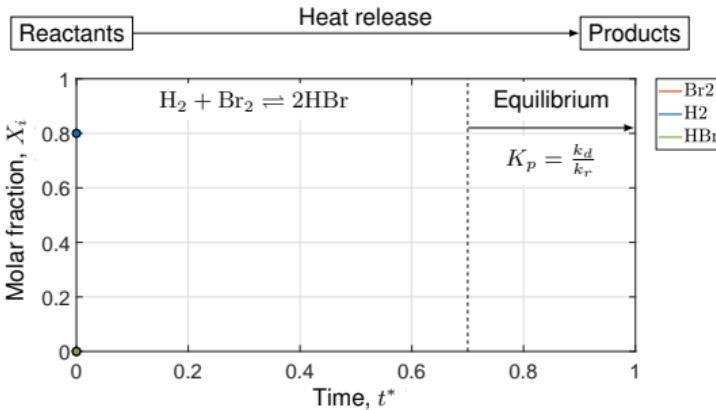
$$dg(T, p, \mathbf{n}) = \sum_{j=1}^{NS} \mu_j(T, p) dn_j = 0,$$

with μ_j the chemical potential of the j th species, namely

$$\mu_j = \left(\frac{\partial g}{\partial n_j} \right)_{T, p, n_k \neq j} .$$

For **ideal gases**, this is the Gibbs free energy of the individual species (do not interact in a mixture).

- Extensive databases of thermochemical properties are required, e.g., **NASA's database**.



We have also a set of restrictions given by the mass balance:

$$h_i = \sum_{j=1}^{NS} \underbrace{a_{ij} n_j}_{b_i} - b_i^\circ = 0 \quad \text{for } i = 1, \dots, \text{NE.}$$

$$\underbrace{\begin{pmatrix} 0 & 2 & 1 \\ 2 & 0 & 1 \end{pmatrix}}_{A^T} \underbrace{\begin{pmatrix} n_{H_2} \\ n_{Br_2} \\ n_{HBr} \end{pmatrix}}_n - \underbrace{\begin{pmatrix} b_{Br}^\circ \\ b_H^\circ \end{pmatrix}}_{b^\circ} = 0.$$

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Constrained minimization with only equality constraints. **Lagrange multipliers.**

$$G(T, p, \mathbf{n}, \boldsymbol{\lambda}) = g(T, p, \mathbf{n}) \pm \boldsymbol{\lambda} (h(T, p, \mathbf{n}) - C),$$

$$\nabla g(T, p, \mathbf{n}) = -\boldsymbol{\lambda} \nabla h(T, p, \mathbf{n}),$$

$$dG(T, p, \mathbf{n}, \boldsymbol{\lambda}) = 0.$$

Many of the equations are not linear → **Newton-Raphson method** (NS + NE + 1 equations)

$$\Delta \ln n_j + \sum_{i=1}^{NE} a_{ij} \frac{\lambda_i}{RT} - \Delta \ln n = -\frac{\mu_j}{RT} \quad (j = 1, \dots, NG),$$

$$\sum_{i=1}^{NE} a_{ij} \frac{\lambda_i}{RT} = -\frac{\mu_j}{RT} \quad (j = NG + 1, \dots, NS),$$

$$\sum_{j=1}^{NG} a_{ij} n_j \Delta \ln n_j + \sum_{j=NG+1}^{NS} a_{ij} \Delta n_j = b_i^\circ - b_i \quad (i = 1, \dots, NE),$$

$$\sum_{j=1}^{NG} n_j \Delta \ln n_j - n \Delta \ln n = n - \sum_{j=1}^{NG} n_j.$$



Main features

- Robust kernel based on Lagrange multipliers.
- Calculation of equilibrium properties of ideal plasmas.
- Up-to-date thermodynamic data (NASA's 9-coefficient polynomial fit).
- Computation of standard chemical equilibrium problems.
- Shock calculations:
 - pre-shock and post-shock states,
 - incident or reflected shocks,
 - Chapman-Jouguet detonations and overdriven detonations, ...
- Operation through command line and GUI.
- Screen and .xls file format output.

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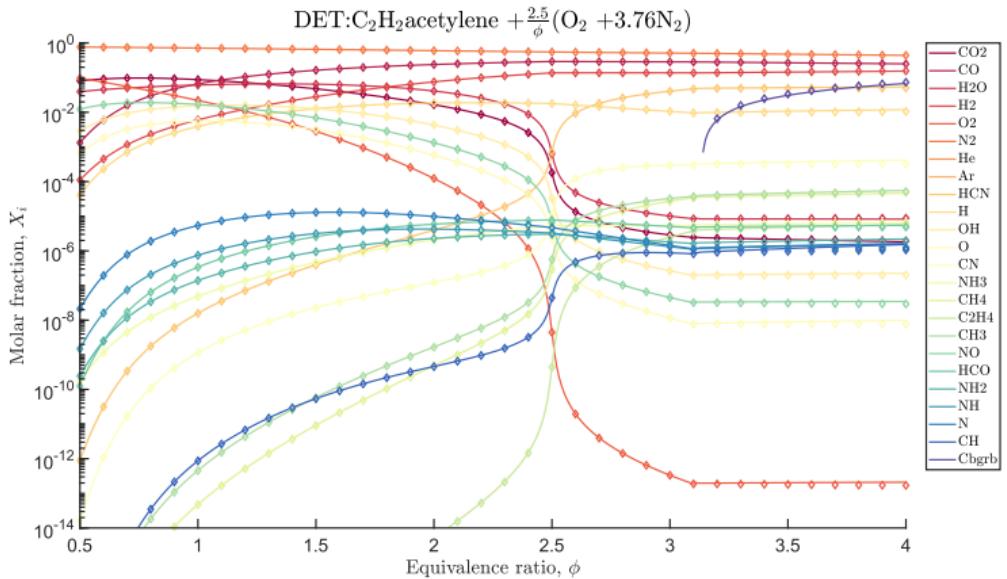
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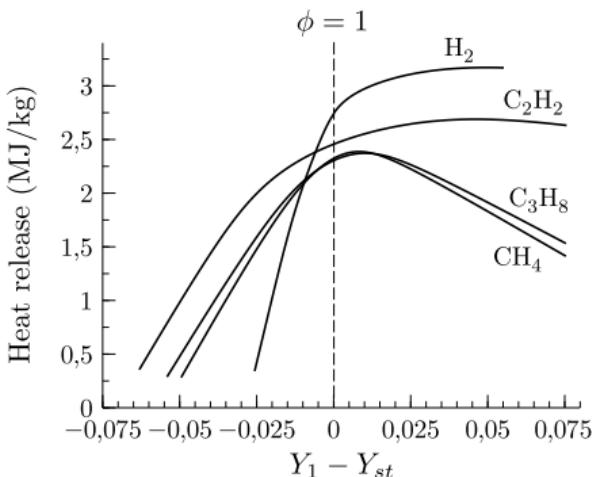
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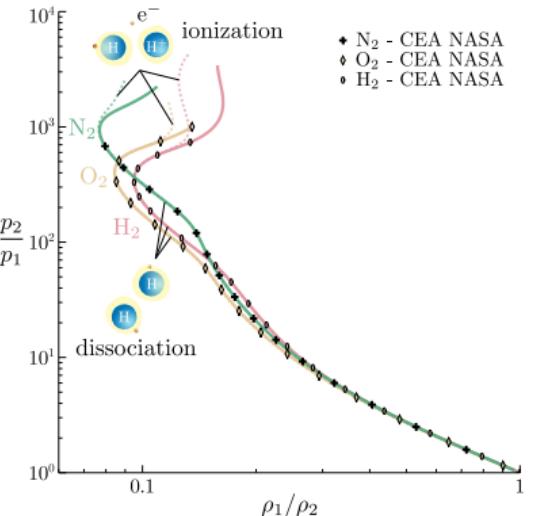


Detonations



E.g., computation of the heat release.

Strong Shocks



E.g., computation of the jump conditions.

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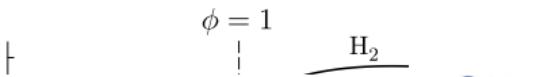
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Detonations



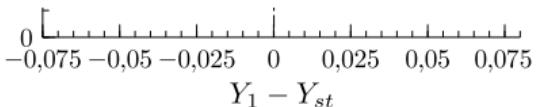
J. Fluid Mech. (2020), vol. 903, A30. © The Author(s), 2020.
Published by Cambridge University Press
doi:10.1017/jfm.2020.651

Effect of equivalence ratio fluctuations on planar detonation discontinuities

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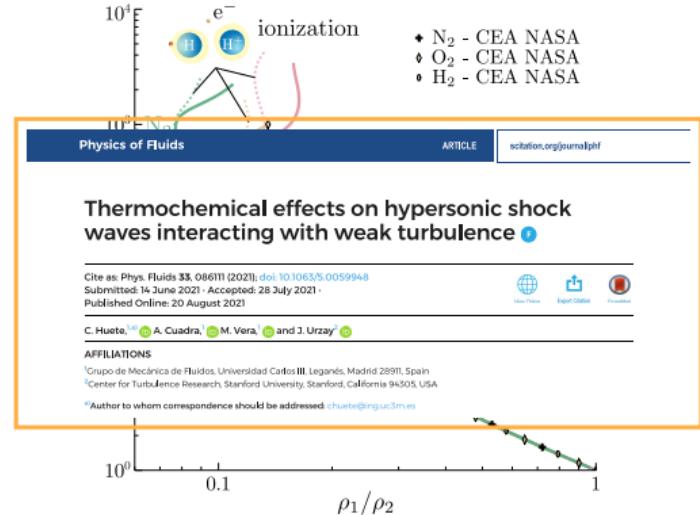
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(Received 13 April 2020; revised 18 June 2020; accepted 29 July 2020)



E.g., computation of the heat release.

Strong Shocks



E.g., computation of the jump conditions.

Conclusion I

Key takeaways

- Combustion toolbox is an **open-source** tool for solving gaseous combustion problems under the **ideal gases** assumption. Allows to include **ideal plasmas**.
- The tool is equipped with an **user-friendly GUI** (standalone, no need MATLAB's license). A great complement for educational purposes.
- In it's **transition to Python**, 100% open-source.
- The plain code is ideal for more sophisticated tasks.
- The overall performance of the code is at level of other thermochemical equilibrium codes. **Boost performance in shock calculations** compared with Caltech's SD-Toolbox, which uses CANTERA as kernel.

Get the code



Cuadra, A. et al. (2022). Combustion Toolbox: A MATLAB-GUI based open-source tool for solving gaseous combustion problems. **Work in progress**.



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Part II

Thermochemical effects on hypersonic shock waves interacting with weak turbulence

In colaboration with Javier Urzay, Center for Turbulence Research, Stanford University.



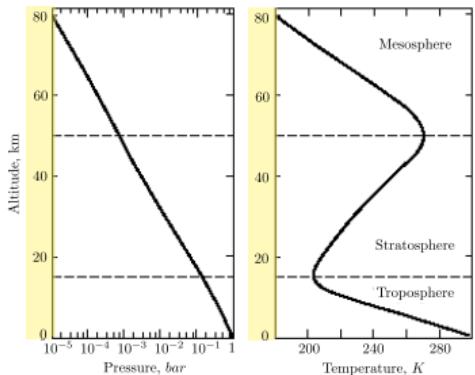
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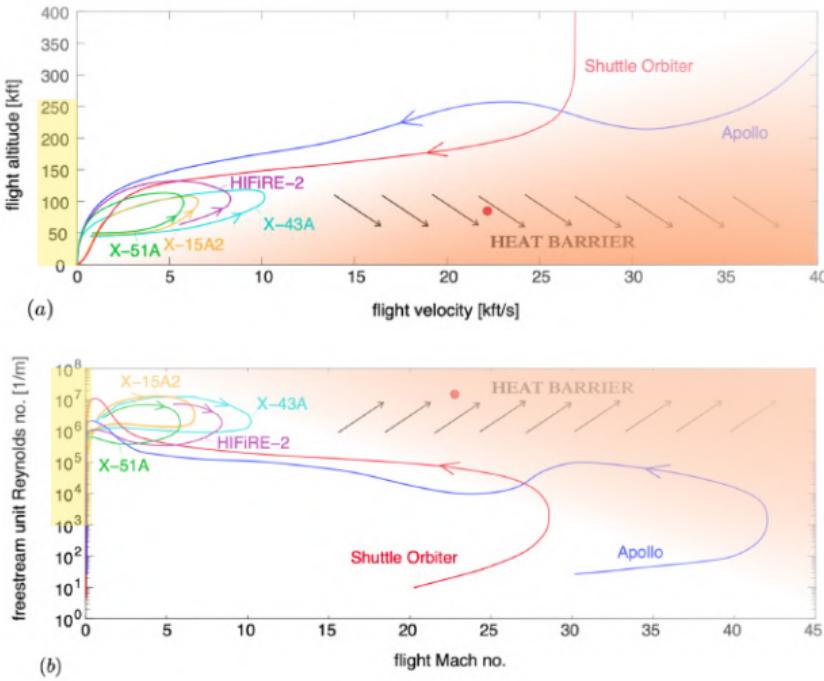
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$$\frac{\Delta p}{p} \sim \frac{\Delta \rho}{\rho} = O(10^5), \quad \frac{\Delta T}{T} = O(1).$$

In hypersonic flight near the ground, the Reynolds number becomes large because of the comparatively larger densities

$$\frac{\Delta Re}{Re} = O(10^5).$$



Urzay, J., & Di Renzo, M. (2021). Annual Research Briefs, Center for Turbulence Research, 7-32.

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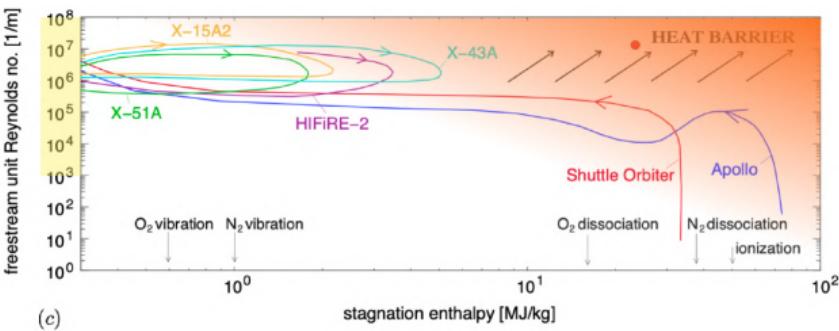
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Urzay, J., & Di Renzo, M. (2021). Annual Research Briefs, Center for Turbulence Research, 7-32.

Hypersonic flight **at low altitudes** is characterized by:

- High free-stream Mach numbers $Ma \geq 5$
- High free-stream and post-shock unit Reynolds numbers $Re \sim 10^7 - 10^9 \text{ m}^{-1}$
- High stagnation enthalpies $h_0 \sim 5 - 30 \text{ MJ/kg}$
- Small mean free paths $\lambda \sim 0.1 \mu\text{m}$
- large normal Mach numbers
- turbulent boundary layers
- much higher than the vibrational specific energies of O_2 and N_2
- short vibrational relaxation distances

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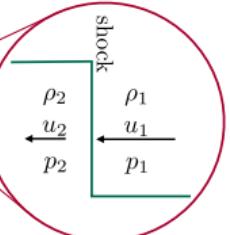
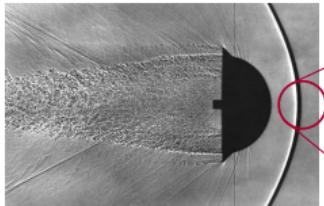
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Integral conservation equations accross shock waves in **dissociating** gases

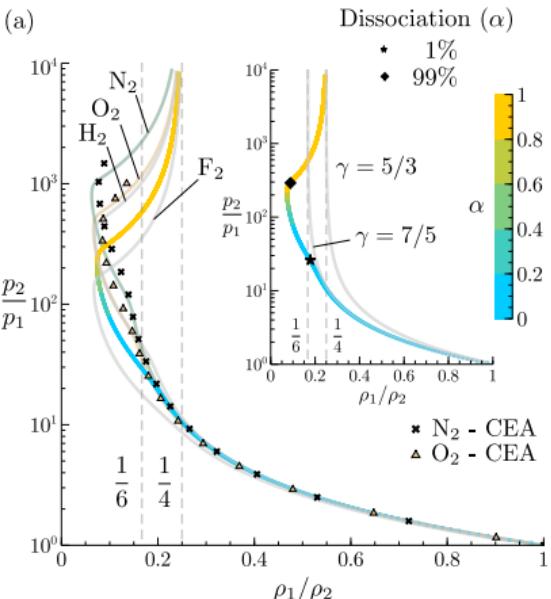
$$\rho_1 u_1 = \rho_2 u_2,$$

$$p_1 + \rho_1 u_1^2 = p_2 + \rho_2 u_2^2,$$

$$e_1 + p_1/\rho_1 + u_1^2/2 = e_2 + p_2/\rho_2 + u_2^2/2 + q_d,$$

Upstream flow is sufficiently cold to be approximated as

$$e_1 = (5/2)R_{g,A_2}T_1, \quad p_1 = \rho_1 R_{g,A_2} T_1.$$



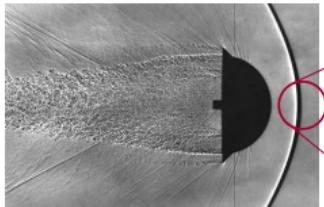
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Integral conservation equations accross shock waves in **dissociating** gases

$$\rho_1 u_1 = \rho_2 u_2,$$

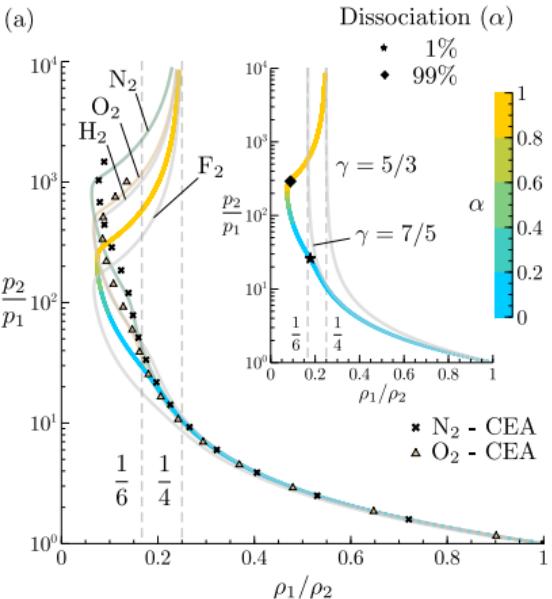
$$p_1 + \rho_1 u_1^2 = p_2 + \rho_2 u_2^2,$$

$$e_1 + p_1/\rho_1 + u_1^2/2 = e_2 + p_2/\rho_2 + u_2^2/2 + q_d,$$

$$p_2 = \rho_2 R_{g,A_2} T_2 (1 + \alpha), \quad q_d = \alpha R_{g,A_2} \Theta_d,$$

$$e_2 = R_{g,A_2} T_2 \left[3\alpha + (1 - \alpha) \left(\frac{5}{2} + \frac{\Theta_v/T_2}{e^{\Theta_v/T_2} - 1} \right) \right],$$

$$\frac{\alpha^2}{1 - \alpha} = Gm\Theta_r \left(\frac{\pi m k_B}{\hbar^2} \right)^{3/2} \frac{\sqrt{T_2}}{\rho_2} e^{-\frac{\Theta_d}{T_2}} \left(1 - e^{-\frac{\Theta_v}{T_2}} \right),$$



where α is the **degree of dissociation**, defined as the mass fraction of A atoms in the reaction $A_2 \rightleftharpoons A + A$, that must be solved with the aid of the chemical equilibrium condition.

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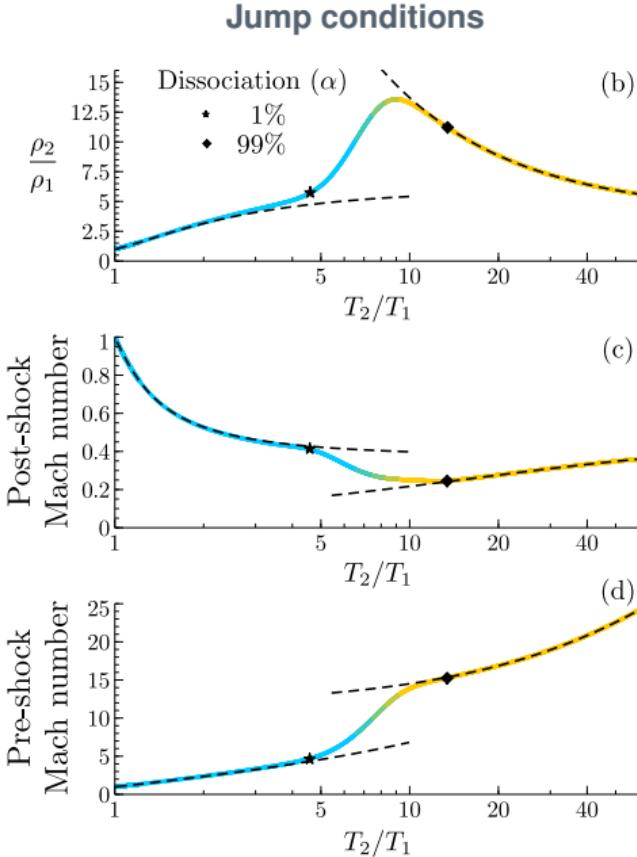
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Endothermicity due to dissociation and vibrational excitation does the following:

- increases the mean post-shock density
- decreases the mean post-shock velocity
- decreases the mean post-shock Mach number
- decreases the mean post-shock temperature



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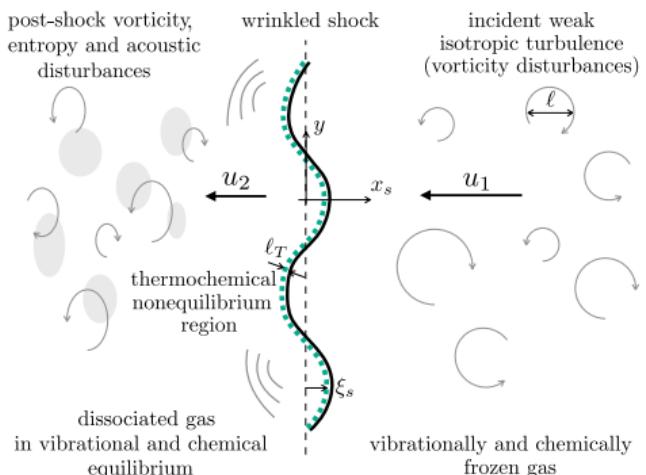
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Considering:

- turbulence is comprised of small fluctuations,
- Kovasznay decomposition into vortical, entropic and acoustic modes,

we can solve this problem analytically by using

- linearized Rankine-Hugoniot relations,
- linearized Euler equations in the post-shock gas.



Limits of validity

Assumptions standard LIA:

- $\text{rms}(u_\ell) \ll a_1$ and a_2 ,
- $\xi_s \ll \ell$,
- $\ell/u_\ell \ll \ell^2/\nu$.

With thermochemical effects:

- $\ell_T \ll \ell$

For a given ℓ , this condition becomes increasingly more accurate as the altitude decreases.

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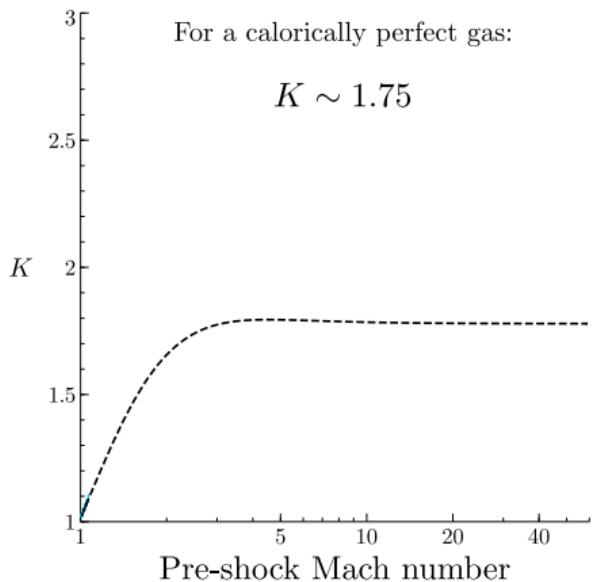
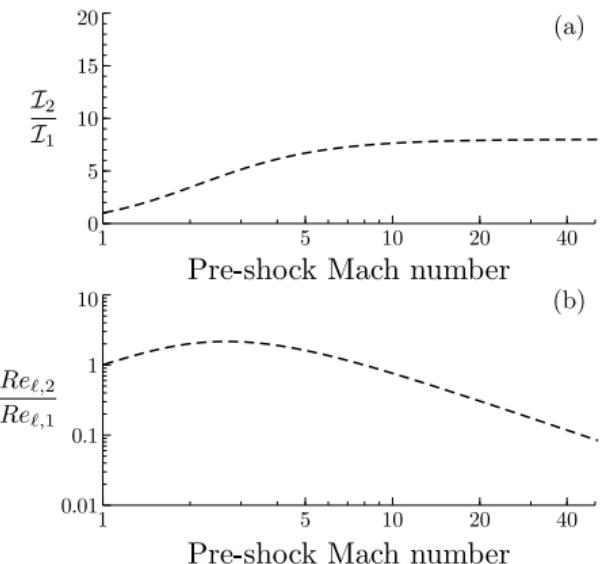
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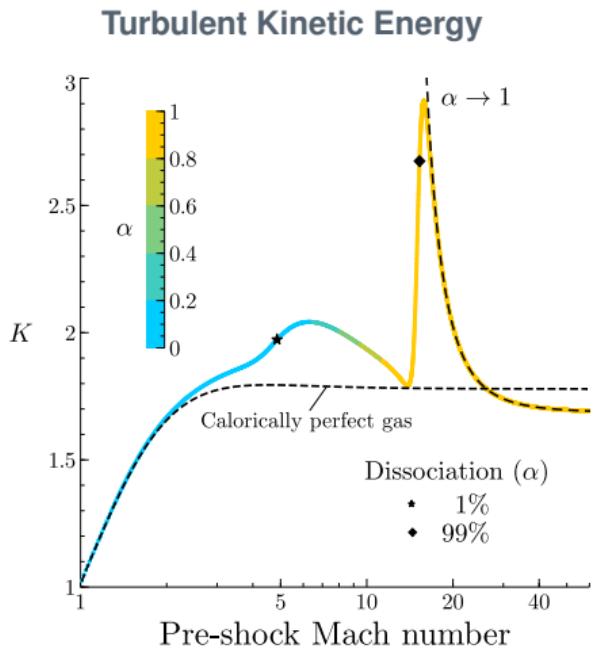
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Turbulent Kinetic Energy**Turbulence intensity and Turbulent Reynolds number**

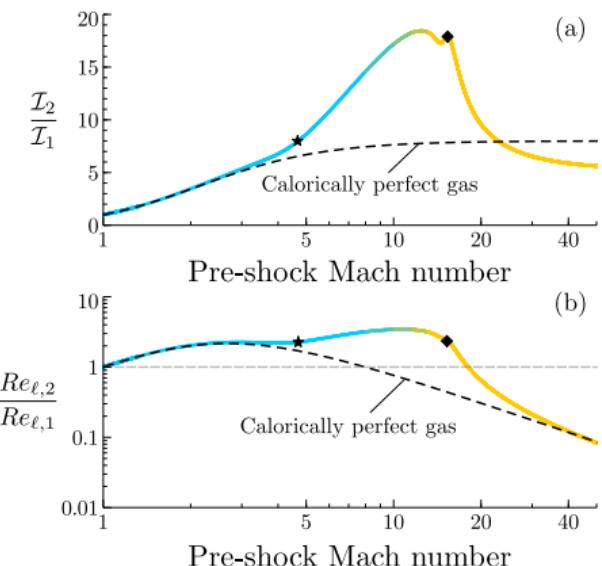
At hypervelocities ($Ma \gtrsim 10$), the calorically perfect gas approximation predicts a saturation in the amplification of kinetic energy and turbulence intensity, along with a decrease in the turbulent Reynolds number across the shock.



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Turbulence intensity and Turbulent Reynolds number

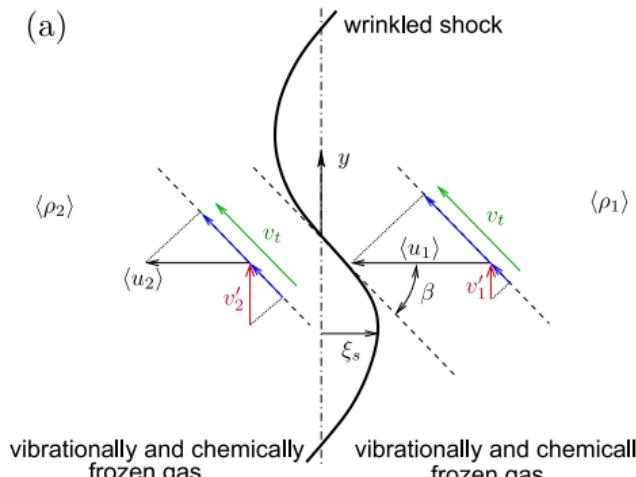


In contrast, the incorporation of dissociation and vibrational excitation predicts larger kinetic energy and turbulence intensity amplification rates, along with an increase in the turbulent Reynolds number across the shock.

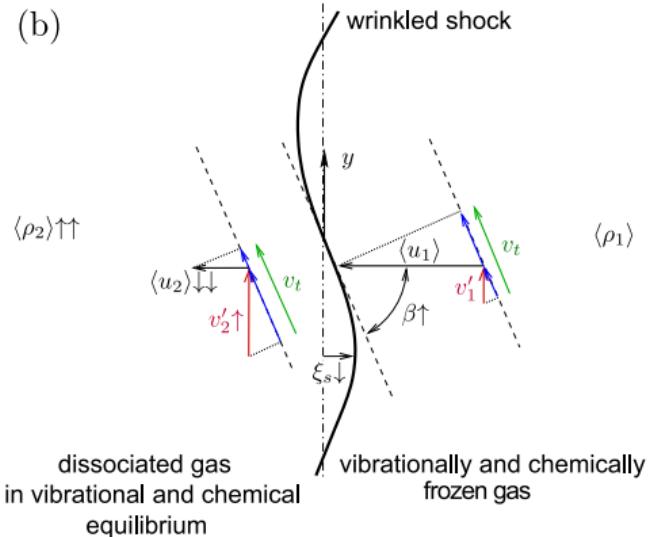
Calorically perfect gas

Vibrationally Excited, Dissociating Gas

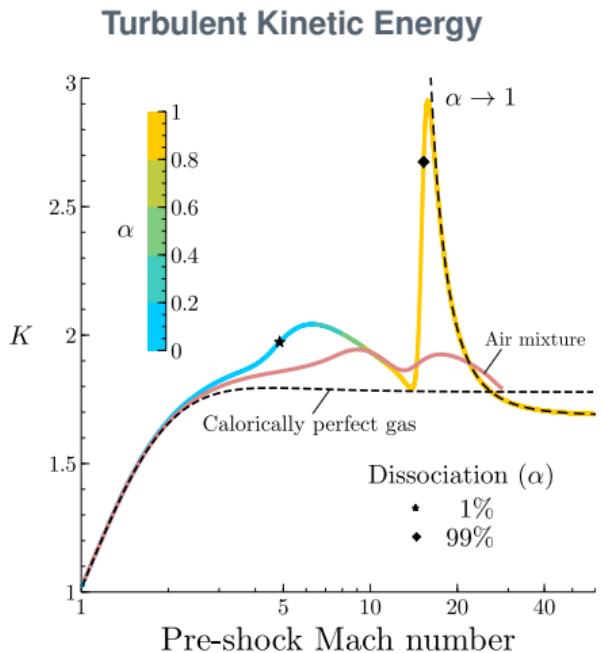
(a)



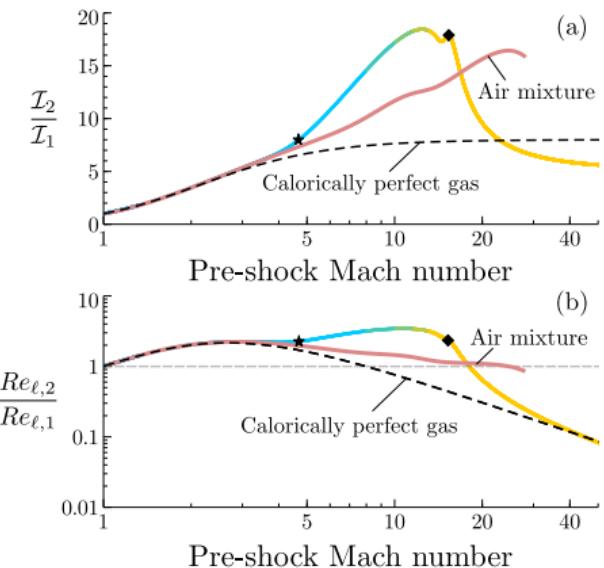
(b)



Conservation of tangential momentum dictates that the transverse velocity fluctuations should increase across the shock – these are larger at hypersonic velocities because of the associated larger post-shock densities induced by endothermic thermochemical effects.



Turbulence intensity and Turbulent Reynolds number



In case of a real air mixture (recombination in multi-species gas and electronic excitation) there is a significant decrease of the peaks values of TKE. However, the qualitative picture remains intact.



Key takeaways

- Significant departures from calorically perfect gas behaviour can be observed in the solution even at modest degrees of dissociation of 1%.
- The amplification of TKE doubles that observed in calorically perfect gases, with most of the content of TKE downstream in form of vortical modes.
- The turbulent Reynolds number is amplified across the shock at hypersonic Mach numbers in the presence of dissociation and vibrational excitation, as opposed to the attenuation observed in the calorically perfect case.
- Preliminary results show that real air mixture share qualitative results, but with lower amplitudes.
- Thermochemical effects arising at hypersonic velocities appear to enhance turbulent fluctuations in the post-shock gas.



Huete, C. et al. (2021). Thermochemical effects on hypersonic shock waves interacting with weak turbulence. *Physics of Fluids*, 33(8), 086111



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